

TD1

How to get the files ?

Download: <http://dms.mat.mines-paristech.fr/Programme/Module-B2/> codes_matlab.tar

- Open a terminal and go to your homedirectory « perso » `=== > cd`
- Create a new repertory `===== > mkdir TD_EF`
- Go in TD_EF `===== > cd perso/TD_EF`

- Move « codes_matlab.tar » in TD_EF
& extract (uncompress) files `===== > tar xvf codes_matlab.tar`

How to run the programs ?

Matlab code repertory `==== in ==== > perso/TD_EF/codes_matlab`

Run matlab code: `cd perso/TD_EF/code_matab`
 `./matlab ./`

GMSH repertory `==== in ==== > perso/TD_EF/gmsh-1.60.1`

Run GMSH: `cd /usr/local/gmsh-1.60.1/`
 `./gmsh`

Introduction

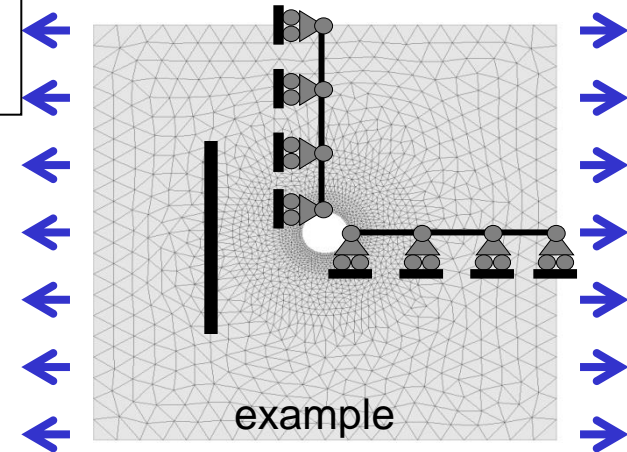
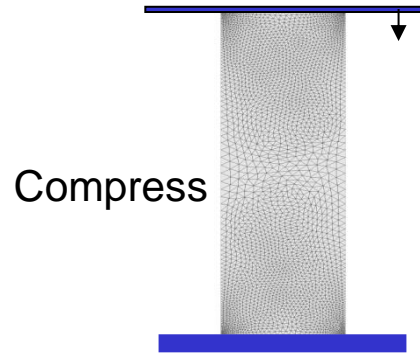
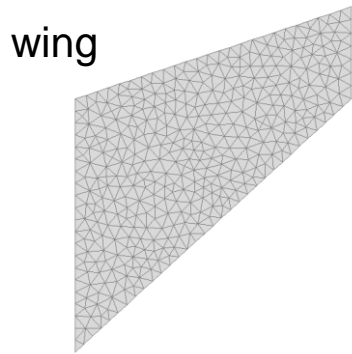
Go to matlab codes directory :
Run matlab:

```
cd perso/TD_EF/codes_matlab  
./matlab ./
```

- **Some examples: Input file** (perso/TD_EF/codes_matlab/input) :

- 3 types of files:

- *.geo: input file gms (geometric description)
- *.msh: output file gms (Mesh description)
- *.inp: input file matlab_code



- **Tutorial code**

`linel_T.m`

(« pedagogical » version)

Main programm.

Run the code:

linel_T (on the matlab command window)

`linel_T_fast.m`

(« faster » version of linel_T)

Main steps ...

1- Geometric description of the structure: == > input/file.geo

Users:

- *geometric definition*
- *physical line, surface*
- *mesh refinement parameter*

2- Mesh generation: == > input/file.msh

Gmsh:

- run gmsh and open file.geo
- Options: mesh, 2D, *first order (T3) ou second order (T6)*
- save (== > file.msh)

3- Problem definition == > input/file.inp

Users :

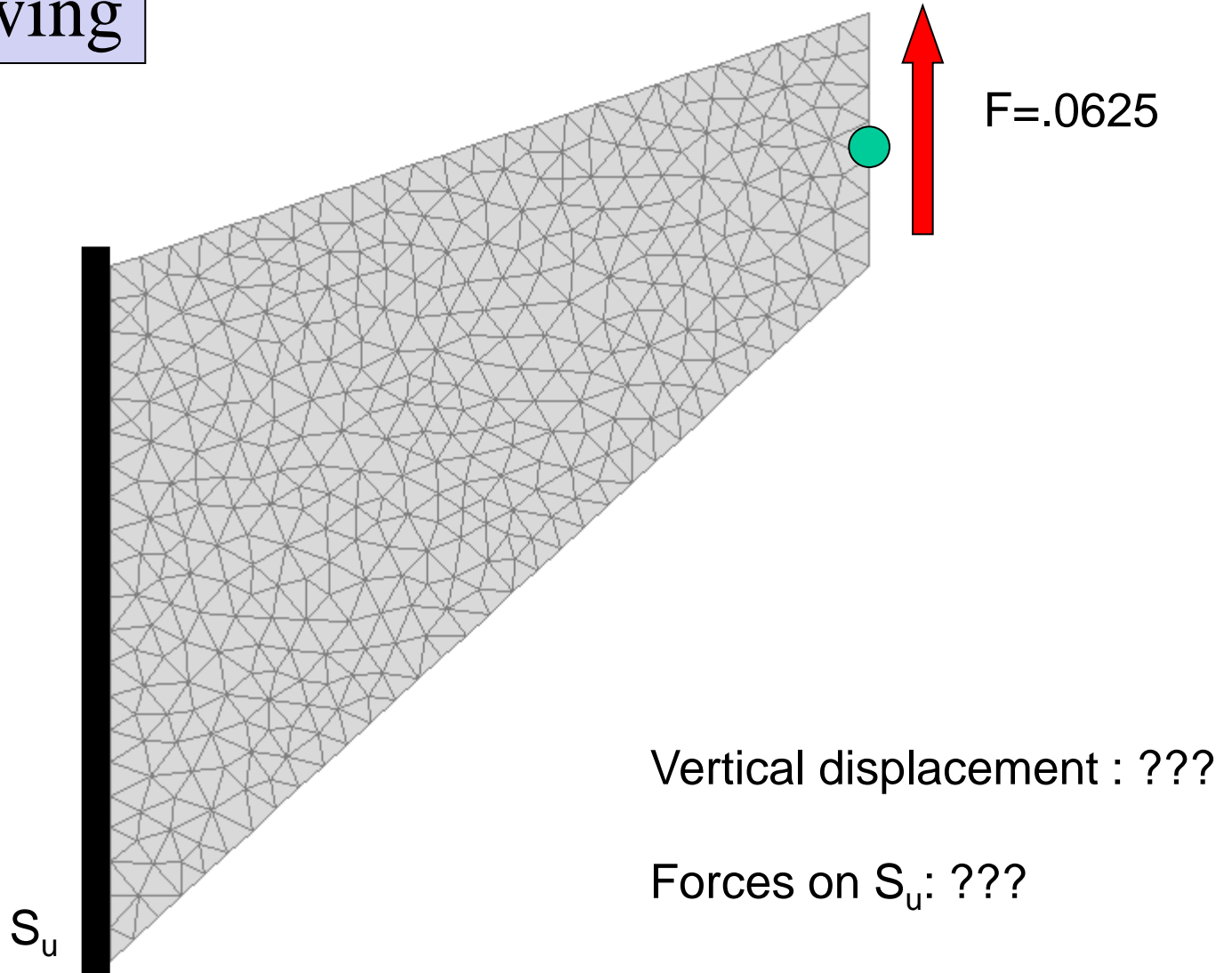
- *define the problem to be solved*
(static, dynamic, ..., material properties, boundary conditions)

4- Compute the Finite Element approximation

Matlab: - run `line1_T` or `line1_T_fast`

Airplane wing: a simplify model !

Airplane wing



Mesh generation: wing.geo

Input file : input/wing.geo

Mesh refinement parameter

wing.geo

```
lc1 = 20;  
  
Point (1) = {0.0,0.0,0.0,lc1};  
Point (2) = {48.0,44.0,0.0,lc1};  
Point (3) = {48.0,60.0,0.0,lc1};  
Point (4) = {0.0,44.0,0.0,lc1};  
  
Line (1) = {1,2};  
Line (2) = {2,3};  
Line (3) = {3,4};  
Line (4) = {4,1};  
Line Loop (5) = {1,2,3,4};  
  
Plane Surface (1) = {5};  
  
Physical Line (1) = {2};  
Physical Line (2) = {4};  
Physical Surface (3) = {1};
```

Line 4 (4,1)

Physical line(2)

Line 3 (3,4)

Line Loop (5) = {1,2,3,4}

Physical Surface(1)={3}

Line 1 (1,2)

Line 2 (2,3)

Physical line(1)

Physical Line (Boundary conditions)

- Physical Line(1) : (traction force)
Line 2: given traction force
- Physical Line(2) : (displacement)
Line 4: embedding (imposed displacement)

Mesh generation: wing.geo

wing.geo

Mesh refinement parameter

```
lc1 = 20;  
  
Point(1) = {0.0,0.0,0.0,lc1};  
Point(2) = {48.0,44.0,0.0,lc1};  
Point(3) = {48.0,60.0,0.0,lc1};  
Point(4) = {0.0,44.0,0.0,lc1};  
  
Line(1) = {1,2};  
Line(2) = {2,3};  
Line(3) = {3,4};  
Line(4) = {4,1};  
Line Loop(5) = {1,2,3,4};  
  
Plane Surface(1) = {5};  
  
Physical Line(1) = {2};  
Physical Line(2) = {4};  
Physical Surface(3) = {1};
```

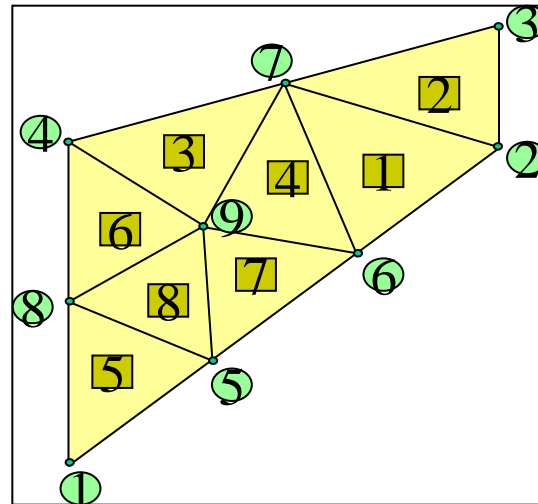
- Run gms : **cd perso/TD_EF/gmsh-1.60.1/**
./gmsh

- open « wing.geo »
- mesh, 2D (Shortcut: esc F3)
- *option: first order (T3) or second order (T6)*
- save (== > generation of wing.msh)

- To modify « input file » == > Edit

TO DO:

- change mesh refinement parameter
- generate the new meshes



Input data: wing.inp

Input file : input/wing.inp

wing.msh

wing.inp

```
*ANALYSIS
STATIC, TYPE=PLANEStress
**
```

Analyse : Static, plane stress

```
*MATERIAL, TYPE=ISOTROPIC
YOUNG=1
POISSON=.3333333
**
```

Material characteristic

```
*SOLID
ELSET=3
**
```

Domain:

ELSET=3 (Physical surface (3))

```
*DBC
ELSET=2, DIR=1, VAL=0.
ELSET=2, DIR=2, VAL=0.
**
```

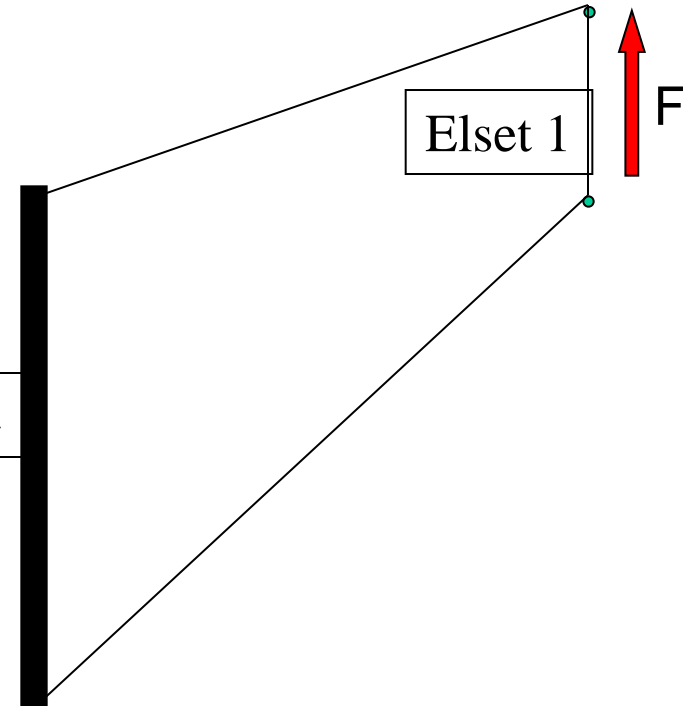
Displacement: DBC

ELSET = 2 (Physical Line(2))
Direction 1 ; Value = 0
Direction 2 ; Value = 0

```
*TBC
ELSET=1, DIR=2, VAL=.0625
**
```

Traction : TBC

ELSET = 1 (Physical Line(1))
Direction 2 :
Value F=0.0625



Input data: wing.inp

wing.geo

wing.msh

```
*ANALYSIS
STATIC, TYPE=PLANESTRESS
**

*MATERIAL, TYPE=ISOTROPIC
YOUNG=1
POISSON=.3333333
**

*SOLID
ELSET=3
**

*DBC
ELSET=2, DIR=1, VAL=0.
ELSET=2, DIR=2, VAL=0.
**

*TBC
ELSET=1, DIR=2, VAL=.0625
**

*ENDFILE
```

Run matlab :

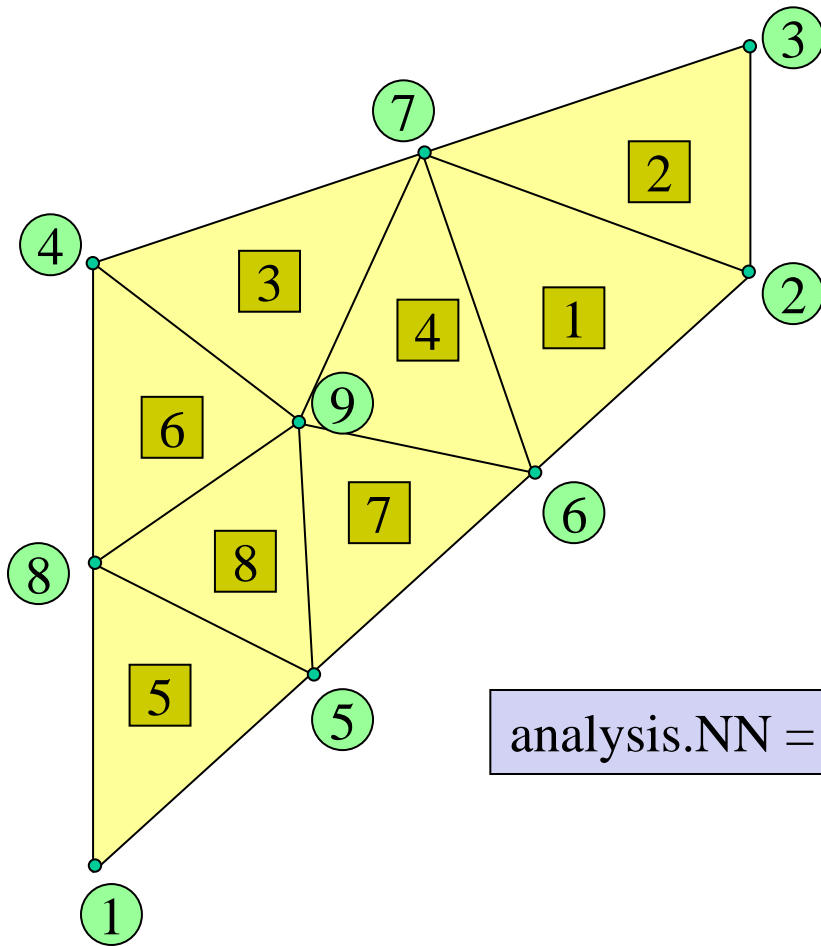
Line1_T.m

But before

... let's have a look on the
main program

Tables: Analysis, materials

```
[analysis materials] connec coor... % reads input file  
dof displ TD]=read_input(pname,fname,t2);
```



analysis.NN = 9

File : utility/read_input.m

```
analysis =
```

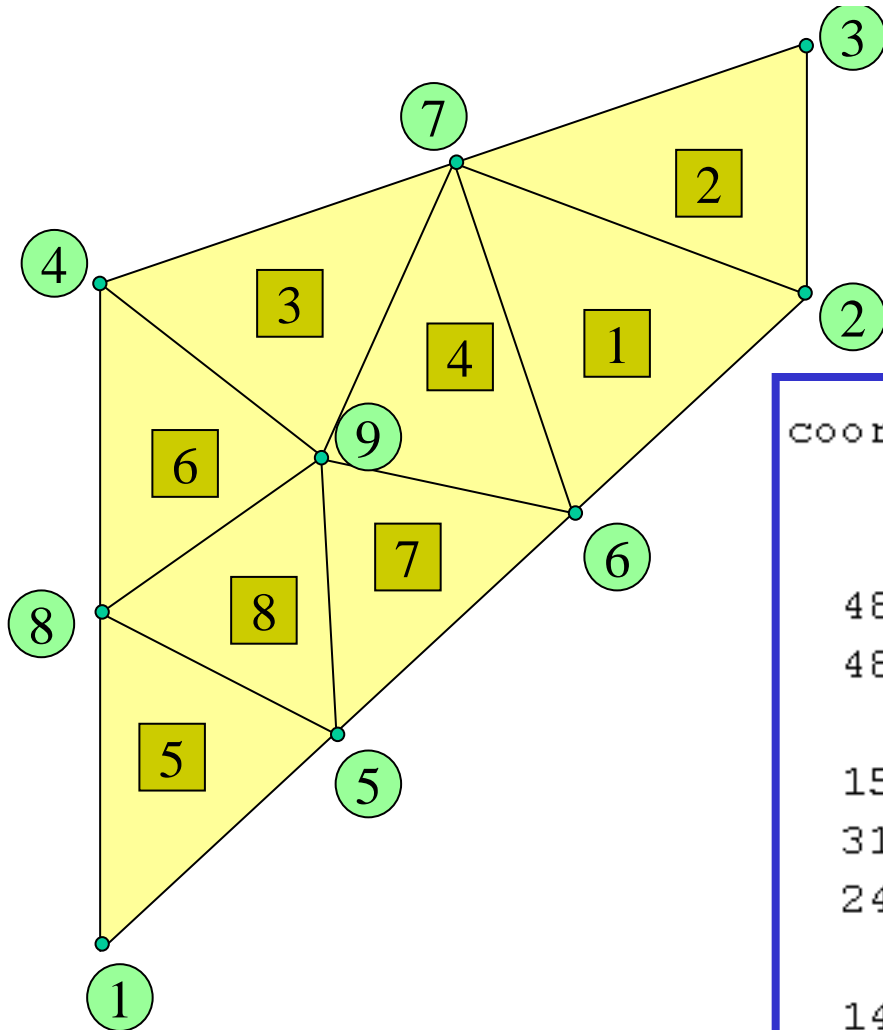
```
NN: 9 # nodes  
NE: 8 # surface elt  
Etag: '3' # '3' ==> T3 ; '6' ==> T6  
ne: 3 #  
ns: 2 #  
ng: 1 # Gauss points  
type: 'PLANEStRESS'  
nTD: 1 # segment (imposed traction)  
neq: 12 # unknown
```

```
materials =
```

```
type: [1x11 char]  
young: 1  
poisson: 0.333333300000000  
A: [3x3 double]
```

Tables: connec, coor

```
[analysis materials connec coor...
dof displ TD]=read_input(pname,fname,t2);
```



```
connec =
```

6	2	7
2	3	7
4	9	7
7	9	6
1	5	8
8	9	4
6	9	5
5	9	8

```
coor =
```

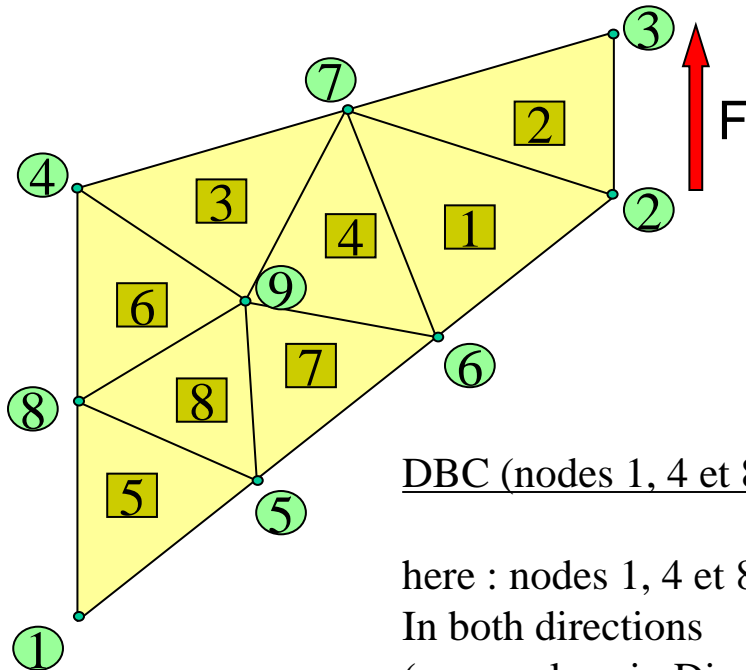
0	0
48.0000000000000000	44.0000000000000000
48.0000000000000000	60.0000000000000000
0	44.0000000000000000
15.9999999999999980	14.6666666666666648
31.9999999999999951	29.3333333333333289
24.0000000000000040	52.0000000000000014
0	22.0000000000000000
14.36198494227833	32.70159631834299

Tables: dof & TD & displ

```
[analysis materials connec coord ...
```

```
% reads input file
```

```
dof displ TD]=read_input(pname,fname,t2);
```



DBC (nodes 1, 4 et 8) :

here : nodes 1, 4 et 8

In both directions

(== > values in Displ)

dof =	
-1	-10
1	2
3	4
-4	-13
5	6
7	8
9	10
-8	-17
11	12

Displ =	
0	0
0	0
0	0
0	0
0	0
0	0
0	0
0	0
0	0

TD (nodes 2 et 3) :

Direction : 2

Value : 0.0625

TD =	
dir:	2
val:	0.0625000000000000
nodes:	[2 3]

Initialisation of the Displacement vector:

- Zero (for unknown dof)
- Value of the imposed displacement for other nodes

Problem formulation

trouver $\underline{u} \in \mathcal{C}(\underline{u}^D)$ tel que

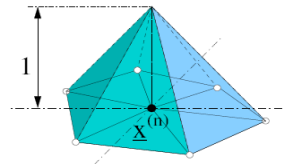
$$\int_{\Omega} \underline{\underline{\varepsilon}}[\underline{u}] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV = \int_{\Omega} \rho \underline{f} \cdot \underline{w} \, dV + \int_{S_T} \underline{T}^D \cdot \underline{w} \, dS \quad \forall \underline{w} \in \mathcal{C}(\underline{0}).$$

$$\underline{u}_h(\underline{x}) = \underline{u}_h^{(D)}(\underline{x}) + \underline{u}_h^{(0)}(\underline{x}) \in \mathcal{C}_h(\underline{u}^D) \quad (\underline{x} \in \Omega_h),$$

$$\text{avec } \underline{u}_h^{(D)}(\underline{x}) = \sum_{(n,j) \mid \text{dof}(n,j)=0} \tilde{N}_n(\underline{x}) u_j^D(\underline{x}^{(n)}) \underline{e}_j \in \mathcal{C}_h(\underline{u}^D)$$

$$\text{et } \underline{u}_h^{(0)} = \sum_{(n,j) \mid \text{dof}(n,j)>0} \tilde{N}_n(\underline{x}) u_j^{(n)} \underline{e}_j \in \mathcal{C}_h(\underline{0});$$

$$\underline{w}(\underline{x}) = \sum_{(n,j) \mid \text{dof}(n,j)>0} \tilde{N}_n(\underline{x}) w_j^{(n)} \underline{e}_j \in \mathcal{C}_h(\underline{0}) \quad (\underline{x} \in \Omega_h).$$



Trouver $\underline{u}_h^{(0)} \in \mathcal{C}_h(\underline{0})$ tel que : $\forall \underline{w} \in \mathcal{C}_h(\underline{0})$,

$$\int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h^{(0)}] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV = - \int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h^{(D)}] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV$$

$$+ \int_{\Omega_h} \underline{f} \cdot \underline{w} \, dV + \int_{S_{T,h}} \underline{T}^D \cdot \underline{w} \, dS.$$

Problem formulation

Trouver $\underline{u}_h^{(0)} \in \mathcal{C}_h(\underline{0})$ tel que : $\forall \underline{w} \in \mathcal{C}_h(\underline{0})$,

$$\int_{\Omega_h} \underline{\underline{\epsilon}}[\underline{u}_h^{(0)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\epsilon}}[\underline{w}] dV = - \int_{\Omega_h} \underline{\underline{\epsilon}}[\underline{u}_h^{(D)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\epsilon}}[\underline{w}] dV + \int_{\Omega_h} \underline{f} \cdot \underline{w} dV + \int_{S_{T,h}} \underline{T}^D \cdot \underline{w} dS.$$

1-
$$\int_{\Omega_h} \underline{\underline{\epsilon}}[\underline{u}_h^{(0)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\epsilon}}[\underline{w}] dV = \sum_{e=1}^{N_E} \int_{E_e} \underline{\underline{\epsilon}}[\underline{u}_h^{(0)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\epsilon}}[\underline{w}] dV$$

$$\int_{E_e} \underline{\underline{\epsilon}}[\underline{u}_h] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\epsilon}}[\underline{w}] dV = \{\underline{W}_e\}^T [\underline{K}_e] \{\underline{U}_e\}$$

avec
$$[\underline{K}_e] = \int_{\Delta_e} [\underline{B}_e(\underline{a})]^T [\underline{A}] [\underline{B}_e(\underline{a})] J_e(\underline{a}) dV(\underline{a})$$

2-
$$\int_{\Omega_h} \underline{\underline{\epsilon}}[\underline{u}_h^{(D)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\epsilon}}[\underline{w}] dV = \sum_{e=1}^{N_E} \int_{E_e} \underline{\underline{\epsilon}}[\underline{u}_h^{(D)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\epsilon}}[\underline{w}] dV$$

Local stiffness matrix: Ke
 Directory: ElementName
 Program : Stiff_line_**ElementName**.m

3-
$$\int_{\Omega_h} \underline{f} \cdot \underline{w} dV + \int_{S_{T,h}} \underline{T}^D \cdot \underline{w} dS.$$

Local extrenal forces: Fe
 Directory: ElementName
 Program : nf_traction_**ElementName**.m

$$\int_{E_e} \underline{f} \cdot \underline{w} dV + \int_{\Gamma_T^e} \underline{T}^D \cdot \underline{w} dS = \{\underline{W}_e\}^T \{\underline{F}_e^{\text{vol}} + \underline{F}_e^{\text{surf}}\} = \{\underline{W}_e\}^T \{\underline{F}_e^{\text{ext}}\}$$

Local stiffness matrix

Local Stiffness Matrix: K_e

Directory: ElementName

Program : Stiff_line1_ElementName.m

$$\int_{E_e} \underline{\underline{\epsilon}}[\underline{u}_h] : \mathcal{A} : \underline{\underline{\epsilon}}[\underline{w}] dV = \{W_e\}^T [K_e] \{U_e\}$$

$$\text{avec } [K_e] = \int_{\Delta_e} [B_e(\underline{a})]^T [A] [B_e(\underline{a})] J_e(\underline{a}) dV(\underline{a})$$

$$\approx \sum_{g=1} w_g [B_e(\underline{a}_g)]^T [A] [B_e(\underline{a}_g)] J_e(\underline{a}_g)$$

```
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
% Linear elastic stiffness matrix: T3
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
function Ke=stiff_line1_T3(T,A)

x11=T(1,1); x21=T(2,1); x31=T(3,1);
x12=T(1,2); x22=T(2,2); x32=T(3,2);
S=.5*((x21-x11)*(x32-x12)-...
      (x31-x11)*(x22-x12));
Be=[x22-x32,0,x32-x12,0,x12-x22,0;
    0,x31-x21,0,x11-x31,0,x21-x11;
    x31-x21,x22-x32,x11-x31, ...
    x32-x12,x21-x11,x12-x22]/(2*S);
Ke=S*Be'*A*Be;
```

```
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
% Linear elastic stiffness matrix: T6
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
function Ke=stiff_line1_T6(T,A)

a_gauss=1/6*[4 1 1; 1 4 1; 1 1 4];
w_gauss=[1/6 1/6 1/6];
Ke=zeros(12,12);
for g=1:3,
    a=a_gauss(g,:);
    DN=[4*a(1)-1 0 -4*a(3)+1 4*a(2) ...
        -4*a(2) 4*(a(3)-a(1));
        0 4*a(2)-1 -4*a(3)+1 4*a(1) ...
        4*(a(3)-a(2)) -4*a(1)];
    J=T'*DN;
    detJ=J(1,1)*J(2,2)-J(1,2)*J(2,1);
    invJ=1/detJ*[ J(2,2) -J(1,2); ...
                 -J(2,1) J(1,1)];
    GN=DN*invJ;
    Be=[GN(1,1) 0 GN(2,1) 0 GN(3,1) 0 ...
        GN(4,1) 0 GN(5,1) 0 GN(6,1) 0;
        0 GN(1,2) 0 GN(2,2) 0 GN(3,2) ...
        0 GN(4,2) 0 GN(5,2) 0 GN(6,2);
        GN(1,2) GN(1,1) GN(2,2) GN(2,1) ...
        GN(3,2) GN(3,1) GN(4,2) GN(4,1) ...
        GN(5,2) GN(5,1) GN(6,2) GN(6,1)];
    Ke=Ke+Be'*A*Be*detJ*w_gauss(g);
end
```

Local external forces

Local external forces : F_e

Directory: ElementName
Program : nf_traction_**ElementName**.m

$$\int_{\Gamma_T^e} \underline{T}^D \cdot \underline{w} \, dS = \{W_e\}^T \left\{ \int_{\Sigma} [N(\underline{b})]^T \{ \underline{T}^D(\underline{x}(\underline{b})) \} \hat{J}(\underline{b}) \, db_1 db_2 \right\} = \{W_e\} \{F_e^{\text{surf}}\}$$

```
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
% Nodal forces due to surface tractions:
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
function Fe=nf_tractions_T3(L,val,idir)

x11=L(1,1); x12=L(1,2);
x21=L(2,1); x22=L(2,2);
H=sqrt((x21-x11)^2+(x22-x12)^2);
NL=H/2*[1 0 1 0;
        0 1 0 1];
TD=zeros(2,1);
if idir>0,
    TD(idir)=val;
else
    n=[(x22-x12); -(x21-x11)]/H;
    TD=val*n;
end
Fe=NL'*TD;
```

Pressure loading : idir=0

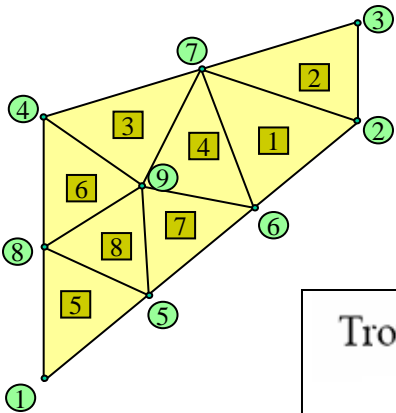
```
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
% Nodal forces due to surface tractions: T6
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
function Fe=nf_tractions_T6(L,val,idir)

a_gauss=[-1/sqrt(3) 1/sqrt(3)];
w_gauss=[1 1];
Fe=zeros(6,1);
for g=1:2
    a=a_gauss(g);
    DN=[a-.5 a+.5 -2*a];
    J=DN*L;
    detJ=sqrt(J(1)^2+J(2)^2);
    TD=zeros(2,1);
    if idir>0,
        TD(idir)=val;
    else
        TD=val/detJ*[J(2) -J(1)]';
    end
    NL=[.5*a*(a-1) .5*a*(1+a) 1-a^2];
    N=[NL(1) 0 NL(2) 0 NL(3) 0;
       0 NL(1) 0 NL(2) 0 NL(3)];
    Fe=Fe+N'*TD*detJ*w_gauss(g);
end
```

Assembly

Trouver $\underline{u}_h^{(0)} \in \mathcal{C}_h(\underline{0})$ tel que : $\forall \underline{w} \in \mathcal{C}_h(\underline{0})$,

$$\int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h^{(0)}] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV = - \int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h^{(D)}] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV + \int_{\Omega_h} \underline{f} \cdot \underline{w} \, dV + \int_{S_{T,h}} \underline{T}^D \cdot \underline{w} \, dS.$$



$$\{\mathbf{W}\} = \{w_1^{(2)}, w_2^{(2)}, w_1^{(3)}, w_2^{(3)}, w_1^{(5)}, w_2^{(5)}, w_1^{(6)}, w_2^{(6)}, w_1^{(7)}, w_2^{(7)}, w_1^{(9)}, w_2^{(9)}\}^T$$

$$\{\mathbf{U}\} = \{u_1^{(2)}, u_2^{(2)}, u_1^{(3)}, u_2^{(3)}, u_1^{(5)}, u_2^{(5)}, u_1^{(6)}, u_2^{(6)}, u_1^{(7)}, u_2^{(7)}, u_1^{(9)}, u_2^{(9)}\}^T$$

Trouver $\{\mathbf{U}\} \in \mathbb{R}^N$ tel que : $\forall \{\mathbf{W}\} \in \mathbb{R}^N$, $\{\mathbf{W}\}^T [\mathbf{K}] \{\mathbf{U}\} = \{\mathbf{W}\}^T \{\mathbf{F}\}$,

$$\{\mathbf{W}\}^T [\mathbf{K}] \{\mathbf{U}\} = \sum_{e=1}^{N_E} \int_{E_e} \underline{\underline{\varepsilon}}[\underline{u}_h^{(0)}] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV,$$

$$\{\mathbf{W}\}^T \{\mathbf{F}\} = \sum_{e=1}^{N_E} \left\{ - \int_{E_e} \underline{\underline{\varepsilon}}[\underline{u}_h^{(D)}] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV + \int_{E_e} \underline{f} \cdot \underline{w} \, dV + \int_{\Gamma_T^e} \underline{T}^D \cdot \underline{w} \, dS \right\}$$

$$\Rightarrow [K]\{U\} = \{F\} \quad \text{with } \{F\} = \{F^{vol}\} + \{F^{surf}\} + \{F^U\}$$

Assembly

Trouver $\underline{u}_h^{(0)} \in \mathcal{C}_h(\underline{0})$ tel que : $\forall \underline{w} \in \mathcal{C}_h(\underline{0})$,

$$\int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h^{(0)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV = - \int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h^{(D)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV + \int_{\Omega_h} \underline{f} \cdot \underline{w} \, dV + \int_{S_{T,h}} \underline{T}^D \cdot \underline{w} \, dS.$$



$$[K]\{U\} = \{F\}$$

with

$$\{F\} = \{F^{vol}\} + \{F^{surf}\} + \{F^U\}$$

1-
$$\int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h^{(0)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV = \sum_{e=1}^{N_E} \int_{E_e} \underline{\underline{\varepsilon}}[\underline{u}_h^{(0)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV$$

Contribution to the global stiffness matrix: $[K]$

$$\int_{E_e} \underline{\underline{\varepsilon}}[\underline{u}_h] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV = \{W_e\}^T [K_e] \{U_e\}$$

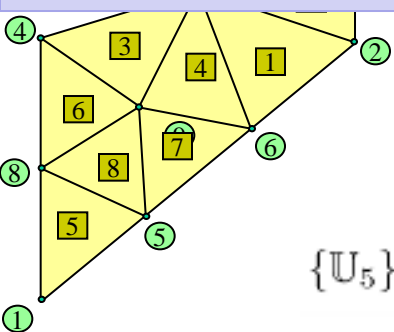
avec
$$[K_e] = \int_{\Delta_e} [B_e(\underline{a})]^T [A] [B_e(\underline{a})] J_e(\underline{a}) \, dV(\underline{a})$$

Contribution to the global right hand side (imposed displacement): $\{F^u\}$

2-
$$\int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h^{(D)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV = \sum_{e=1}^{N_E} \int_{E_e} \underline{\underline{\varepsilon}}[\underline{u}_h^{(D)}] : \underline{\underline{\mathcal{A}}} : \underline{\underline{\varepsilon}}[\underline{w}] \, dV$$

Boundary condition: displacement

Example : Element 5



Trouver $\underline{u}_h^{(0)} \in \mathcal{C}_h(\Omega)$ tel que : $\forall \underline{w} \in \mathcal{C}_h(\Omega)$,

$$\int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h^{(0)}] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{w}] dV = - \int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h^{(D)}] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{w}] dV + \int_{\Omega_h} \underline{f} \cdot \underline{w} dV + \int_{S_{T,h}} \underline{T}^D \cdot \underline{w} dS.$$

$$\{\mathbf{U}_5\} = \left\{ u_1^{(D1)}, u_2^{(D1)}, u_1^{(5)}, u_2^{(5)}, u_1^{(D8)}, u_2^{(D8)} \right\}^T \quad \{\mathbf{W}_5\} = \{0, 0, w_1^{(5)}, w_2^{(5)}, 0, 0\}^T$$

$$\{\mathbf{U}_5^{(D)}\} = \{u_1^{(D1)}, u_2^{(D1)}, u_1^{(D8)}, u_2^{(D8)}\}^T$$

$$\{\mathbf{U}_5^{(0)}\} = \{u_1^{(5)}, u_2^{(5)}\}^T$$

$$\{\mathbf{W}_5^{(0)}\} = \{w_1^{(5)}, w_2^{(5)}\}^T$$

$$\{\mathbf{W}_{e=5}\}^T [\mathbf{K}_{e=5}] \{\mathbf{U}_{e=5}\} = \left\{ 0 \quad 0 \quad \begin{bmatrix} w_1^{(5)} & w_2^{(5)} \end{bmatrix} \quad 0 \quad 0 \right\}$$

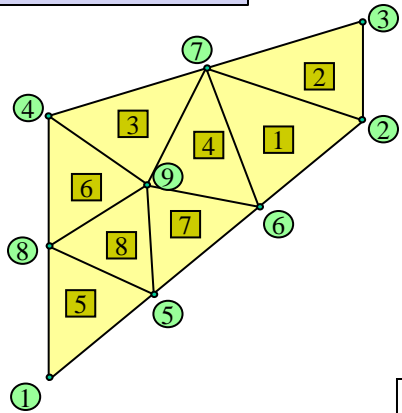
$K_{e=5}^{(11)}$	$K_{e=5}^{(12)}$	$K_{e=5}^{(13)}$	$K_{e=5}^{(14)}$	$K_{e=5}^{(15)}$	$K_{e=5}^{(16)}$	$\left. \begin{array}{l} U_1^{(1)} \\ U_2^{(1)} \\ U_1^{(5)} \\ U_2^{(5)} \\ U_1^{(8)} \\ U_1^{(8)} \end{array} \right\}$
$K_{e=5}^{(21)}$	$K_{e=5}^{(22)}$	$K_{e=5}^{(23)}$	$K_{e=5}^{(24)}$	$K_{e=5}^{(25)}$	$K_{e=5}^{(26)}$	
$K_{e=5}^{(31)}$	$K_{e=5}^{(32)}$	$K_{e=5}^{(33)}$	$K_{e=5}^{(34)}$	$K_{e=5}^{(35)}$	$K_{e=5}^{(36)}$	
$K_{e=5}^{(41)}$	$K_{e=5}^{(42)}$	$K_{e=5}^{(43)}$	$K_{e=5}^{(44)}$	$K_{e=5}^{(45)}$	$K_{e=5}^{(46)}$	
$K_{e=5}^{(51)}$	$K_{e=5}^{(52)}$	$K_{e=5}^{(53)}$	$K_{e=5}^{(54)}$	$K_{e=5}^{(55)}$	$K_{e=5}^{(56)}$	
$K_{e=5}^{(61)}$	$K_{e=5}^{(62)}$	$K_{e=5}^{(63)}$	$K_{e=5}^{(64)}$	$K_{e=5}^{(65)}$	$K_{e=5}^{(66)}$	

$$\{\mathbf{W}_{e=5}\}^T [\mathbf{K}_{e=5}] \{\mathbf{U}_{e=5}\} = \left\{ \mathbf{W}_{e=5}^0 \right\}^T \begin{bmatrix} K_{e=5}^{(33)} & K_{e=5}^{(34)} \\ K_{e=5}^{(43)} & K_{e=5}^{(44)} \end{bmatrix} \left\{ \mathbf{U}_{e=5}^0 \right\} + \left\{ \mathbf{W}_{e=5}^0 \right\}^T \begin{bmatrix} K_{e=5}^{(31)} & K_{e=5}^{(32)} & K_{e=5}^{(35)} & K_{e=5}^{(36)} \\ K_{e=5}^{(41)} & K_{e=5}^{(42)} & K_{e=5}^{(45)} & K_{e=5}^{(46)} \end{bmatrix} \left\{ \mathbf{U}_{e=5}^D \right\}$$

$$\{\mathbf{W}_5\}^T [\mathbf{K}_5] \{\mathbf{U}_5\} = \left\{ \mathbf{W}_5^{(0)} \right\}^T [\mathbf{K}_5^{(00)}] \left\{ \mathbf{U}_5^{(0)} \right\} + \left\{ \mathbf{W}_5^{(0)} \right\}^T [\mathbf{K}_5^{(0D)}] \left\{ \mathbf{U}_5^{(D)} \right\}$$

Boundary condition: displacement

Element 5



$$\{W_{e=5}\}^T [K_{e=5}] \{U_{e=5}\} = \begin{Bmatrix} 0 \\ 0 \\ w_1^{(5)} \\ w_2^{(5)} \\ 0 \\ 0 \end{Bmatrix}^T \begin{bmatrix} K_{e=5}^{(11)} & K_{e=5}^{(12)} & K_{e=5}^{(13)} & K_{e=5}^{(14)} & K_{e=5}^{(15)} & K_{e=5}^{(16)} \\ K_{e=5}^{(21)} & K_{e=5}^{(22)} & K_{e=5}^{(23)} & K_{e=5}^{(24)} & K_{e=5}^{(25)} & K_{e=5}^{(26)} \\ K_{e=5}^{(31)} & K_{e=5}^{(32)} & K_{e=5}^{(33)} & K_{e=5}^{(34)} & K_{e=5}^{(35)} & K_{e=5}^{(36)} \\ K_{e=5}^{(41)} & K_{e=5}^{(42)} & K_{e=5}^{(43)} & K_{e=5}^{(44)} & K_{e=5}^{(45)} & K_{e=5}^{(46)} \\ K_{e=5}^{(51)} & K_{e=5}^{(52)} & K_{e=5}^{(53)} & K_{e=5}^{(54)} & K_{e=5}^{(55)} & K_{e=5}^{(56)} \\ K_{e=5}^{(61)} & K_{e=5}^{(62)} & K_{e=5}^{(63)} & K_{e=5}^{(64)} & K_{e=5}^{(65)} & K_{e=5}^{(66)} \end{bmatrix} \begin{Bmatrix} U_1^{(1)} \\ U_2^{(1)} \\ U_1^{(5)} \\ U_2^{(5)} \\ U_1^{(8)} \\ U_1^{(8)} \end{Bmatrix}$$

$$\{W_5\}^T [K_5] \{U_5\} = \{W_5^{(0)}\}^T [K_5^{(00)}] \{U_5^{(0)}\} + \{W_5^{(0)}\}^T [K_5^{(0D)}] \{U_5^{(D)}\}$$

```

nodes=convec(e,:)
dofe=dof(nodes,:)

dofe=reshape(dofe',[1,6])
pe=find(dofe>0);
Ie=dofe(pe);
K(Ie,Ie)=K(Ie,Ie)+Ke(pe,pe);
pe_UDe=find(dofe<0);
Ie_UDe=-dofe(pe_UDe);
UDE=displ(Ie_UDe)';
F(Ie)=F(Ie)-Ke(pe,pe_UDe)*UDE
    
```

```

nodes=[1 5 8]
dofe=[-1 -10;
      5 6;
      -8 -17]
dofe=[-1 -10 5 6 -8 -17]
pe=[3 4]; Local numbering
Ie=[5 6]; Global numbering
pe_UDe=[1 2 5 6];
Ie_UDe=[1 10 8 17];
UDE=[0 0 0 0];
    
```

Contribution to [K]

dof =	
-1	-10
1	2
3	4
-4	-13
5	6
7	8
9	10
-8	-17
11	12

Contribution to {F}

Matlab translation ...

```

D=2;
Dne=D*analysis.ne;
Dns=D*analysis.ns;
for e=1:analysis.NE,
    nodes=conec(e,:);
    T=coor(nodes,:);
    Ke=eval(['stiff_line1_T',analysis.Etag,...
            '(T,materials.A)']);
    dofe=reshape(dof(nodes,:),[1,Dne]);
    pe=find(dofe>0);
    Ie=dofe(pe);
    K(Ie,Ie)=K(Ie,Ie)+Ke(pe,pe);
    pe_UEde=find(dofe<0);
    Ie_UEde=-dofe(pe_UEde);
    UDe=displ(Ie_UEde)';
    F(Ie)=F(Ie)-Ke(pe,pe_UEde)*UDe;
end
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% assemblage phase: nodal loads due to surfac
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
for s=1:analysis.nTD,
    nodes=TD(s).nodes;
    idir=TD(s).dir;
    val=TD(s).val;
    L=coor(nodes,:);
    Fe=eval(['nf_tractions_T',analysis.Etag,...
            '(L,val,idir)']);
    dofs=reshape(dof(nodes,:),[Dns,1]);
    ps=find(dofs>0);
    Is=dofs(ps);
    F(Is)=F(Is)+Fe(ps);
end
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Solution phase
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
U=K\F;
clear K F
    
```

```

analysis =
    NN: 9
    NE: 8
    Etag: '3'
    ne: 3
    ns: 2
    ng: 1
    type: 'PLANESTRESS'
    nTD: 1
    neq: 12
    
```

conec =		
6	2	7
2	3	7
4	9	7
7	9	6
1	5	8
8	9	4
6	9	5
5	9	8

```
Ke=stiff_line1_T3(T,materials.A);
```

Displacement boundary condition

dof =	
-1	-10
1	2
3	4
-4	-13
5	6
7	8
9	10
-8	-17
11	12

```
Fe=nf_tractions_T3(L,val,idir);
```

Post traitement: Cauchy Stress components

Directory : ElementName
 Program : StressG_line1_ElementName.m

$$\{\underline{\underline{\epsilon}}[v_h](\underline{x})\} = [B_e(\underline{a})]\{V_e\}, \quad \{\sigma\} = [A]\{\epsilon\}.$$

```

%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
% Stresses in one T3 element due to displa
% elastic constitutive law
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
function stressG=stressG_line1_T3(T,A,Ve)

x11=T(1,1); x21=T(2,1); x31=T(3,1);
x12=T(1,2); x22=T(2,2); x32=T(3,2);
S=.5*((x21-x11)*(x32-x12)-...
      (x31-x11)*(x22-x12));
Be=[x22-x32,0,x32-x12,0,x12-x22,0;
     0,x31-x21,0,x11-x31,0,x21-x11;
     x31-x21,x22-x32,x11-x31, ...
     x32-x12,x21-x11,x12-x22]/(2*S);
stressG=(A*Be*Ve)';
  
```

To be compare with stiff_line1_T3 ...

```

%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
% Linear elastic stiffness matrix: T3
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
function Ke=stiff_line1_T3(T,A)

x11=T(1,1); x21=T(2,1); x31=T(3,1);
x12=T(1,2); x22=T(2,2); x32=T(3,2);
S=.5*((x21-x11)*(x32-x12)-...
      (x31-x11)*(x22-x12));
Be=[x22-x32,0,x32-x12,0,x12-x22,0;
     0,x31-x21,0,x11-x31,0,x21-x11;
     x31-x21,x22-x32,x11-x31, ...
     x32-x12,x21-x11,x12-x22]/(2*S);
Ke=S*Be'*A*Be;
  
```

```

%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
% Stresses at gauss points: T6
%!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
function stressG=stressG_line1_T6(T,A,Ve)

a_gauss=1/6*[4 1 1; 1 4 1; 1 1 4];
stressG=zeros(3,3);
for g=1:3,
    a=a_gauss(g,:);
    DN=[4*a(1)-1 0 -4*a(3)+1 4*a(2) ...
        -4*a(2) 4*(a(3)-a(1));
        0 4*a(2)-1 -4*a(3)+1 4*a(1) ...
        4*(a(3)-a(2)) -4*a(1)];
    J=T'*DN;
    detJ=J(1,1)*J(2,2)-J(1,2)*J(2,1);
    invJ=1/detJ*[ J(2,2) -J(1,2); ...
                  -J(2,1) J(1,1)];
    GN=DN*invJ;
    Be=[GN(1,1) 0 GN(2,1) 0 GN(3,1) 0 ...
        GN(4,1) 0 GN(5,1) 0 GN(6,1) 0;
        0 GN(1,2) 0 GN(2,2) 0 GN(3,2) ...
        0 GN(4,2) 0 GN(5,2) 0 GN(6,2);
        GN(1,2) GN(1,1) GN(2,2) GN(2,1) ...
        GN(3,2) GN(3,1) GN(4,2) GN(4,1) ...
        GN(5,2) GN(5,1) GN(6,2) GN(6,1)];
    stressG(g,:)=(A*Be*Ve)';
end
  
```

Post traitement: Cauchy Stress components

Matlab function: `ic = find(dof>0);`
`= >` returns the indices of « dof »
that satisfy the condition

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Post-processing phase: computation of nodal stresses v
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
ic=find(dof>0);           % finds act
displ(ic)=U(dof(ic));    % and copie
stress=zeros(analysis.NN,3); % initializes "stress"
counter=zeros(analysis.NN,1); % initializes "counter"
for e=1:analysis.NE,    % computes nodal stresses
    nodes=connec(e,:);
    T=coor(nodes,:);    % creates element
    Ve=reshape(displ(nodes,:)',[Dne,1]);
    stressG=eval(['stressG_line1_T',... % computes stresses in one element ...
        analysis.Etag,'(T,materials.A,Ve)']); % at gauss points
    stressN=eval(['G2N_T',... % and extrapolates to vertex nodes
        analysis.Etag,'(T,stressG)']);
    stress(nodes,:)=stress(nodes,:)+stressN; % adds stresses to triangle nodes
    counter(nodes)=counter(nodes)+1;
end
for icomp=1:3
    stress(:,icomp)=stress(:,icomp)./counter; % naive average of stresses
end
    
```

```

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Extrapolation from Gauss points to nodes: T6
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
function qN=G2N_T6(T,qG)

N=1/9*[2 -1 -1 4 1 4;
       -1 2 -1 4 4 1;
       -1 -1 2 1 4 4];
xg=[ones(3,1) N*T]; % physical coordinates of gauss points
M=[ones(6,1) T];
qN=M*(xg\qG); % linear extrapolation to nodes
    
```

```

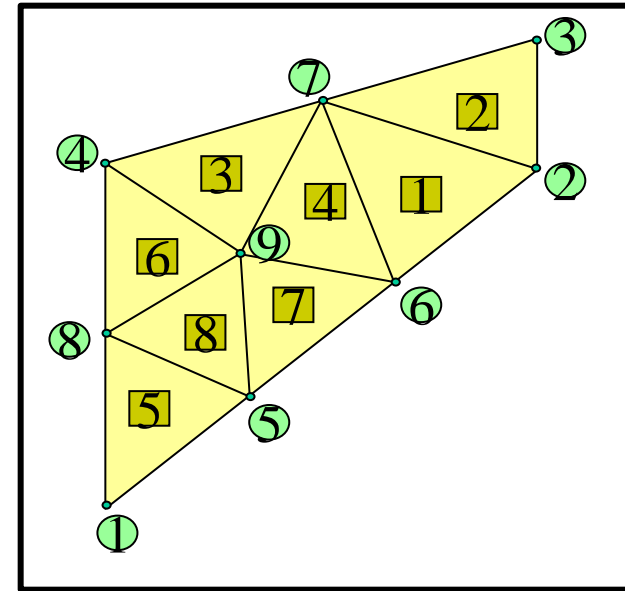
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Extrapolation from Gauss points to nodes: T3
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
function qN=G2N_T3(T,qG)

qN=[qG; qG; qG];
    
```

EX 1: Extract some information

Write matlab code lines:

- To display total number of element
- To display total number of nodes
- To find all nodes that belong to the line $x=0$



Ex 2: Assembly

- 1 - How is compute the coefficients $K(5,7)$, $K(5,10)$ and $K(12,9)$?
 - where does it come from ?
 - which elements contribute to its computation ?
 - which coefficients of K_e contribute to its computation ?
- 2 – What is the contribution of :
 $K_2(1,2)$, $K_4(4,6)$ and $K_5(1,6)$
 - Verify with the code

dof =

```
-1  -10
 1   2
 3   4
-4  -13
 5   6
 7   8
 9  10
-8  -17
11  12
```

connec =

```
6   2   7
2   3   7
4   9   7
7   9   6
1   5   8
8   9   4
6   9   5
5   9   8
```

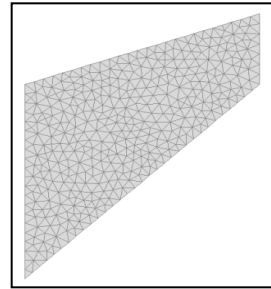
EX 3: Potential energy (DM)

- 1- Matlab code lines to evaluate the potential energy for the FE solution

$$\mathcal{P}(\underline{u}_h) = \frac{1}{2} \int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{u}_h] dV - \int_{\Omega_h} \underline{f} \cdot \underline{u}_h dV - \int_{S_{T,h}} \underline{T}^D \cdot \underline{u}_h dS$$

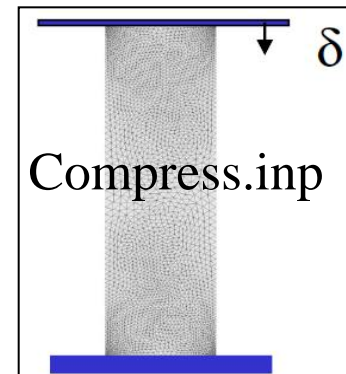
- 2- Convergence analysis (Wing case)

Plot the potential energy in function of the number of elements (mesh refinement) for T3 and T6 elements.



- 3- Compute the potential energy for the example « compress.inp »

wing.inp



Work in pairs

Hand in next session

Send by email: (clement.olivier@safran.fr)

- *Your names*
- *Matlab code lines*
- *1 pages (max) of comments and analysis*

Correction EX 1: extract some information

Write matlab code lines:

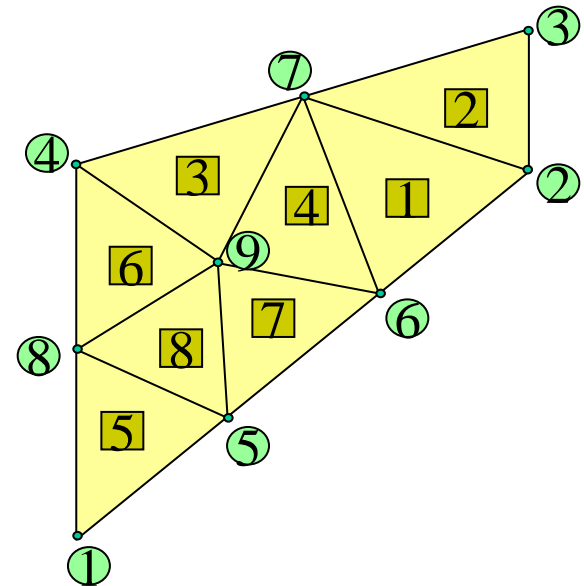
- **To display total number of element:** `== > NbElement = analysis.NE`
or `== > NbElement = size(convec,1)`
- **To display total number of nodes:** `== > NbNodes = analysis.NN`
or `== > NbNodes = size(coor,1)`
- **To find all nodes that belong to the line $x=0$**

```
SX0=find(coor(:,1)<(1.d-4));
```

SX0 =

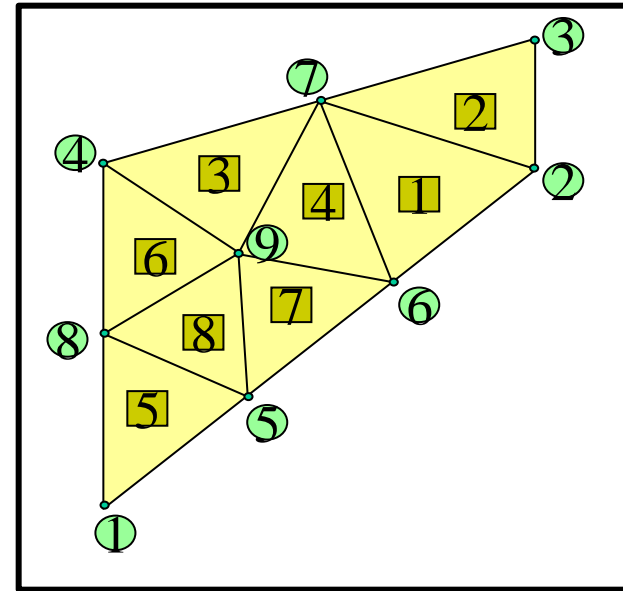
1
4
8

`== > SX0` contains the list
(column) of the nodes that
belong to the line $x=0$



Correction EX 2 – Assembly (1/2)

- 1 - How is compute the coefficient $K(5,7)$, $K(5,10)$ and $K(12,9)$?
 - where does it come from ?
 - which elements contribute to its computation ?
 - which coefficients of K_e contribute to its computation ?



$K(5,7)$

- Node 5 (direction 1) & Node 6 (direction 1)
- Element 7
- $K(1,4) = K_7(5,1)$

- 2 – Same question for $K(5,10)$

$K(5,10)$

- Node 5 (direction 1) & Node 7 (direction 2)
- No common support of shape functions
- $K(5,11) = 0$

- 3 – Same question for $K(12,9)$

- Node 9 (direction 2) & Node 7 (direction 1)
- Elements 3 & 4
- $K(12,9) = K_3(4,5) + K_4(4,1)$

dof =

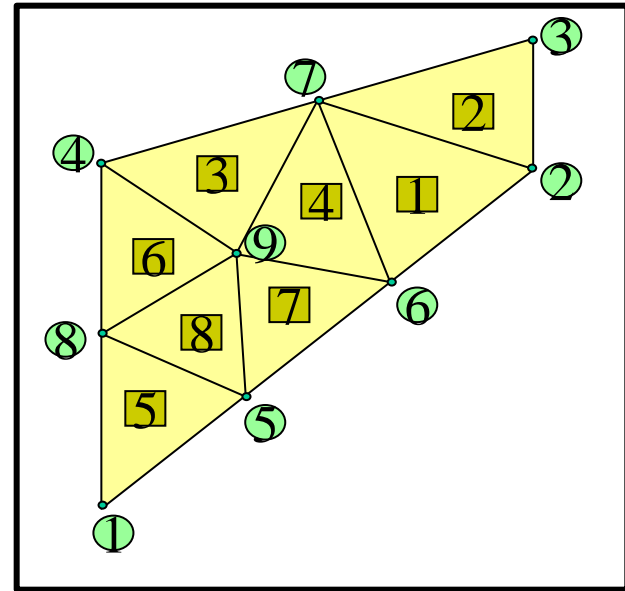
-1	-10
1	2
3	4
-4	-13
5	6
7	8
9	10
-8	-17
11	12

connecc =

6	2	7
2	3	7
4	9	7
7	9	6
1	5	8
8	9	4
6	9	5
5	9	8

Correction EX 2 – Assembly (2/2)

- 2 – What is the contribution of :
 $K_2(1,2)$, $K_4(4,6)$ and [$K_5(2,3)$ and $K_5(3,2)$]



$K_2(1,2)$

- dof_2 = 1 ↔ Node : 2 Dir 1 ↔ dof = 1
- dof_2 = 2 ↔ Node : 2 Dir 2 ↔ dof = 2
- $K(1,2) \leftarrow K_2(1,2)$ (but ≠)

$K_4(4,6)$

- dof_4 = 4 ↔ Node : 9 Dir 2 ↔ dof = 12
- dof_4 = 6 ↔ Node : 6 Dir 2 ↔ dof = 8
- $K(12,8) \leftarrow K_4(4,6)$ (but ≠)

$K_5(3,2)$ and $K_5(2,3)$

- dof_5 = 3 ↔ Node : 5 Dir 1 ↔ dof = 5
- dof_5 = 2 ↔ Node : 1 Dir 2 ↔ dof = -10
- $F^u(5) \leftarrow K_5(3,2) * U^{(1)^2}$ (but ≠)
- $K_5(2,3)$ does not contribute

dof =

-1	-10
1	2
3	4
-4	-13
5	6
7	8
9	10
-8	-17
11	12

connecc =

6	2	7
2	3	7
4	9	7
7	9	6
1	5	8
8	9	4
6	9	5
5	9	8

Hints EX 3: Potential energy

- 1- Matlab code lines to evaluate the potential energy for the FE solution

$$\mathcal{P}(\underline{u}_h) = \frac{1}{2} \int_{\Omega_h} \underline{\underline{\varepsilon}}[\underline{u}_h] : \mathcal{A} : \underline{\underline{\varepsilon}}[\underline{u}_h] dV - \int_{\Omega_h} \underline{f} \cdot \underline{u}_h dV - \int_{S_{T,h}} \underline{T}^D \cdot \underline{u}_h dS$$

Prove:
$$P(\underline{u}_h) = \sum_e \left(\frac{1}{2} \{\mathbf{U}_e\}^T [\mathbf{K}_e] \{\mathbf{U}_e\} - \{\mathbf{U}_e\}^T \{\mathbf{F}_e^{ext}\} \right) = \frac{1}{2} \{\mathbf{U}\}^T [\mathbf{K}] \{\mathbf{U}\} - \{\mathbf{U}\}^T \{\mathbf{F}\} + P(\underline{u}_h^{(D)})$$